# Scuola di Dottorato Leonardo da Vinci – a.a. 2007/08

# LASER: CARATTERISTICHE, PRINCIPI FISICI, APPLICAZIONI

Versione 1 – Luglio 08 – http://www.df.unipi.it/~fuso/dida

# Parte 6 Proprietà della luce laser, emissione impulsata ed impulsi ultra-brevi

#### **SOMMARIO**

Sappiamo che la luce laser ha proprietà uniche (monocromaticità, coerenza, brillanza, etc.) e sappiamo come è fatto un laser

- Proprietà della luce laser e strategie di miglioramento:

monocromaticità coerenza temporale e spaziale brillanza

- Laser ad alta ed altissima intensità (impulsati):

Q-switching mode locking ed impulsi ultra-brevi

Obiettivo : capire l'origine delle proprietà del laser

Obiettivo secondario: discutere alcune strategie per ottimizzare l'operazione laser ed ottenere risultati specifici

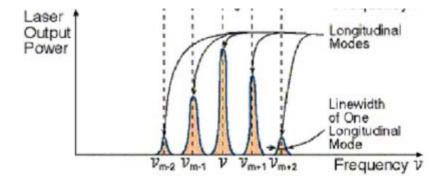
# **MONOCROMATICITÀ**

#### 1.4. PROPERTIES OF LASER BEAMS

Laser radiation is characterized by an extremely high degree of monochromaticity, coherence, directionality, and brightness. We can add a fifth property, viz., short duration, which refers to the capability of producing very short light pulses, a less fundamental but nevertheless very important property. We now consider these properties in some detail.

#### 1.4.1. Monochromaticity

This property is due to the following two circumstances: (1) Only an em wave of frequency  $\nu$  given by Eq. (1.1.1) can be amplified. (2) Since a two-mirror arrangement forms a resonant cavity, oscillation can occur only at the resonance frequencies of this cavity. The latter circumstance leads to an often much narrower laser linewidth (by as much as 10 orders of magnitude) than the usual linewidth of the transition  $2\rightarrow 1$ , as observed in spontaneous emission.



Larghezza di riga del laser regolata da larghezza di riga della cavità Il carattere monocromatico dipende da:

- Selezione singolo modo longitudinale;
- Larghezza del modo (cavità);
- (spesso) selezione modo trasversale

cavita na un anuamento temporate di questo tipo per t≥0

$$E(t) = E(0) e^{-i\omega t - t/2\tau}$$

 $Q = 2\pi\beta c/\lambda = \omega/\beta = \omega \tau$ τ: vita media fotohe<sup>6</sup>n cavità

a partire dal tempo t=0 in cui la radiazione è stata immessa nella cavità.

Esaminiamo ora la distribuzione spettrale di Fourier di questo campo elettrico alla frequenza angolare  $\Omega$ :

$$E(\Omega) = \frac{1}{\sqrt{2\pi}} \int_0^\infty E(t) e^{i\Omega t} dt =$$

$$= \frac{1}{\sqrt{2\pi}} E(0) \int_0^\infty e^{i\left[(\Omega - \omega) + \frac{i}{2\pi}\right] t} dt = \frac{1}{\sqrt{2\pi}} \frac{E(0)}{i\left[(\Omega - \omega) + \frac{i}{2\pi}\right]} \text{ (VIII.2.7)}$$

La intensità u della componente di Fourier del campo elettrico a frequenza  $\Omega$  vale:

$$u(\Omega) = \frac{1}{8\pi} \left| E(\Omega) \right|^2 = \frac{1}{16\pi^2} \frac{\left| E(0) \right|^2}{(\Omega - \omega)^2 + \frac{1}{4\tau^2}}$$
(VIII.2.8)

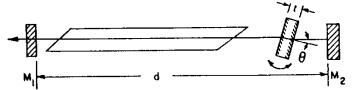
Quindi questa intensità ha una distribuzione spettrale data da una forma Lorentziana con una larghezza a mezza altezza data da:

$$\Delta \omega_{\rm c} = \frac{1}{\tau} = \frac{\omega}{\rm O} \tag{VIII.2.9}$$

Una misura della larghezza della distribuzione spettrale del campo elettrico dentro la cavità permette di determinare il fattore Q della cavità. E' da notare che la larghezza della distribuzione

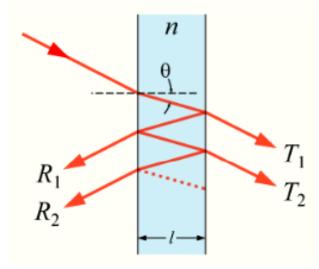
# STRATEGIE DI AUMENTO Q

#### **Intracavity etalon**



In optics, a Fabry-Pérot interferometer or etalon is typically made of a transparent plate with two reflecting surfaces, or two parallel highly reflecting mirrors. (Technically the former is an etalon and the latter is an interferometer, but the terminology is often used inconsistently.) Its transmission spectrum as a function of wavelength exhibits peaks of large transmission corresponding to resonances of the etalon. It is named after Charles Fabry and Alfred Perot. [1] "Etalon" is from the French étalon, meaning "measuring gauge" or "standard". [2]

Fig.5.36. Single-mode operation by inserting a tilted etalon inside the laser resonator



A Fabry-Pérot etalon. Light enters the etalon and undergoes multiple internal reflections.

The phase difference between each succeeding reflection is given by  $\delta$ :

$$\delta = \left(\frac{2\pi}{\lambda}\right) 2nl\cos\theta.$$

If both surfaces have a reflectance R, the transmittance function of the etalon is given by:

$$T_e = \frac{(1-R)^2}{1+R^2-2R\cos(\delta)} = \frac{1}{1+F\sin^2(\frac{\delta}{2})}$$

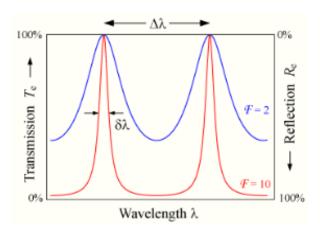
where 
$$F=rac{4R}{(1-R)^2}$$
 is the coefficient of finesse.

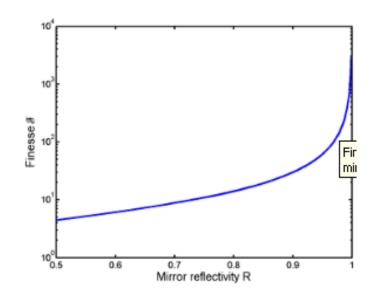
The varying transmission function of an etalon is caused by interference between the multiple reflections of light between the two reflecting surfaces. Constructive interference occurs if the transmitted beams are in phase, and this corresponds to a high-transmission peak of the etalon. If the transmitted beams are out-of-phase, destructive interference occurs and this corresponds to a transmission minimum. Whether the multiply-reflected beams are in-phase or not depends on the wavelength  $(\lambda)$  of the light (in vacuum), the angle the light travels through the etalon  $(\theta)$ , the thickness of the etalon (I) and the refractive index of the material between the reflecting surfaces (n).

#### FINEZZA E LARGHEZZA DI RIGA

$$T_e = \frac{(1-R)^2}{1+R^2 - 2R\cos(\delta)} = \frac{1}{1+F\sin^2(\frac{\delta}{2})}$$

where 
$$F=rac{4R}{(1-R)^2}$$
 is the coefficient of finesse.





Possibile realizzare etalon con finezza > 10<sup>3</sup> (a scapito della trasmissione!)

Larghezze di riga tipiche per laser CW (in continua):

- Laser a gas (HeNe, Ar<sup>+</sup>,...):  $\Delta v < 1$  MHz (anche < 1 kHz per laser con cavità ultrastabili)
- Laser a stato solido (Nd:YAG, TiSa, centri di colore, ...):  $\Delta v \sim 1$  MHz (anche < 10 kHz con etalon)
- Laser a colorante:  $\Delta v \sim 100$  MHz (fino a 100 kHz per laser con etalon)
- Laser a diodo:  $\Delta v \sim 1$  MHz (anche < 10 kHz per laser con cavità esterna)

# LIMITE QUANTISTICO

#### Schawlow-Townes Linewidth

Definition: linewidth of a single-frequency laser with quantum noise only

Even before the first laser was experimentally demonstrated. Schawlow and Townes calculated the fundamental (quantum) limit for the linewidth of a laser [1]. This lead to the famous Schawlow-Townes equation:

Esiste limite quantistico per larghezza di riga dovuto a fluttuazioni quantistiche (em. spont.)

$$\Delta v_{\text{laser}} = \frac{\pi h v (\Delta v_{\text{c}})^2}{P_{\text{out}}}$$

 $\Delta v_{\text{laser}} = \frac{\pi \, h \nu \, (\Delta v_{\text{c}})^2}{P_{\text{out}}}$  Es.: HeNe,  $h \, v$ =2eV,  $\Delta v_{\text{C}}$ =1MHz,  $P_{\text{out}}$ =1mW  $\rightarrow \Delta v_{\text{S.T.}}$ ~1mHz!!

with the photon energy  $h\nu$ , the resonator bandwidth  $\Delta\nu_c$  (full width at half-maximum, FWHM), and the output power Pout. It has been assumed that there are no parasitic cavity losses. (Compared with the original equation, a factor 4 has been removed because of a different definition of the resonator bandwidth.)

It is often claimed that the phase noise level corresponding to the Schawlow-Townes linewidth is a result of spontaneous emission into the laser mode. Although this picture is intuitive, it is not completely correct. Both the laser gain and the linear losses of the laser resonator contribute equal amounts of quantum noise to the intracavity light field. This means that even when replacing laser gain with some noiseless amplification process, the phase noise would only decrease to half of the Schawlow-Townes value [2].

Carefully constructed solid-state lasers can have very small linewidths in the region of a few kilohertz. which is still significantly above their Schawlow-Townes limit: technical excess noise makes it difficult to reach that limit. The linewidth of semiconductor lasers is also normally much larger than according to the original equation (without the  $\alpha$  factor). This, however, is largely caused by amplitude-to-phase coupling effects (which can be quantified with the linewidth enhancement factor), and not by technical excess noise.

Altre fluttuazioni "tecnologiche" (es. fase/ampiezza) generalmente più importanti di limite Schawlow-Townes

# **SINTONIZZABILITÀ**

Lo spettro di guadagno del mezzo attivo ha normalmente larghezze "piccole" (typ. 1-10GHz) → Eventuale sintonizzabilità è selezione dei modi (oppure scelta della riga attiva, e.g. Ar<sup>+</sup>,CO<sub>2</sub>)

Eccezioni: laser con mezzi attivi "a banda larga": -Laser a colorante (in soluzione o allo stato solido -Laser a diodo (bande invece di livelli discreti...)

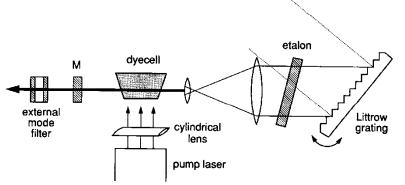
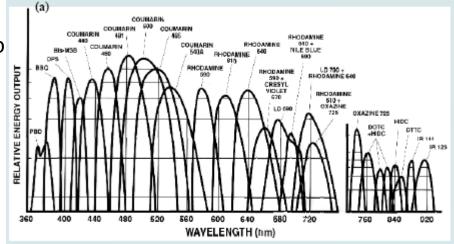


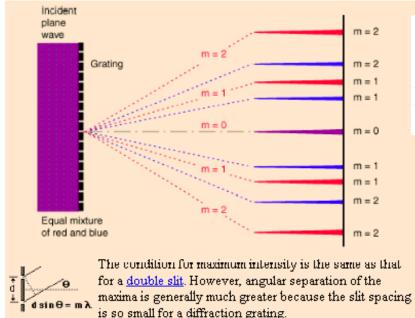
Fig.5.44. Short Hänsch-type dye-laser cavity with Littrow grating and mode selection either with an internal etalon or an external FPI as "mode filter" [5.57]



Cavità terminate da reticolo di diffrazione invece che specchi

When there is a need to separate light of different wavelengths with high resolution, then a diffraction grating is most often the tool of choice. This "super prism" aspect of the diffraction grating leads to application for measuring atomic spectra in both laboratory instruments and telescopes. A large number of parallel, closely spaced slits constitutes a diffraction grating. The condition for maximum intensity is the same as that for the double slit or multiple slits, but with a large number of slits the intensity maximum is very sharp and narrow, providing the high resolution for spectroscopic applications. The peak intensities are also much higher for the grating than for the double slit.

#### **DIFFRACTION GRATINGS**



$$d \sin \theta_m = m\lambda$$
. Tipicamente  $d = 1/3600-1/600 \text{ mm}^{-1}$ 

It is straightforward to show that if a plane wave is incident at an angle  $\theta_i$ , the grating equation becomes

$$d\left(\sin\theta_m + \sin\theta_i\right) = m\lambda.$$

The light that corresponds to direct transmission (or specular reflection in the case of a reflection grating) is called the zero order, and is denoted m = 0. The other maxima occur at angles which are represented by non-zero integers m. Note that m can be positive or negative, resulting in diffracted orders on both sides of the zero order beam.

La diffrazione dal reticolo segue le leggi dell'interferenza da sorgenti (slits) multiple

Riflessione massima ad una determinata combinazione di angoli di incidenza e riflessione

La cavità terminata da un reticolo ha perdite dipendenti dalla lunghezza d'onda

Laser può operare solo se le perdite sono minori del guadagno

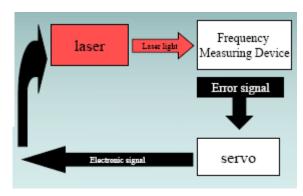
Emissione sintonizzabile

## STABILIZZAZIONE LASER

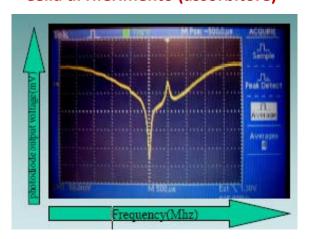
Laser possono essere stabilizzati rispetto a vari parametri (e.g., ampiezza, frequenza)

Strategia di stabilizzazione: feedback elettronico (PID) su riferimento → lunghezza cavità

- The optical frequency of a single-frequency laser, or the frequency of one line of the frequency comb from a mode-locked laser, can be stabilized via resonator length control. The feedback signal can be obtained e.g. by recording a beat note with a second laser, by measuring the transmission or reflection of a very stable reference cavity, or by measuring the transmission of some absorption cell (e.g. an iodine cell), possibly using Doppler-free spectroscopy. A frequently used technique for generating an error signal is the Pound-Drever-Hall method [2, 3], using a weak phase modulation of the light which is sent to a reference cavity. A scheme not requiring such modulation is the Hänsch-Couillaud method [1].

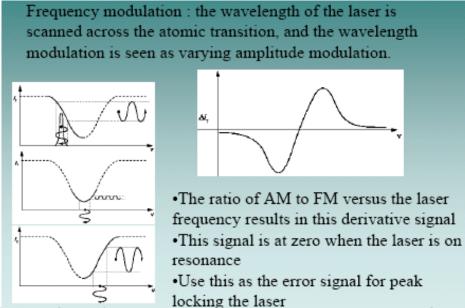


#### Cella di riferimento (assorbitore)



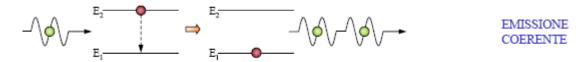
Tecniche di stabilizzazione più raffinate (e.g., Pound-Drever) per arrivare a stabilità 10<sup>-10</sup> -

10<sup>-12</sup> e larghezze di riga < 1Hz (su tempribre vi)<sup>07/08</sup> - Parte 6 - Versione 1



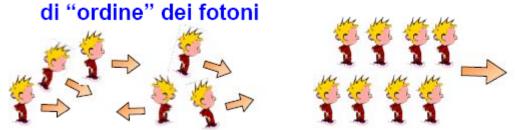
# **PROPRIETÀ LUCE LASER**

- Monocromaticità
- Coerenza (spaziale e temporale)
- Brillanza (intensità e collimazione/focalizzazione)

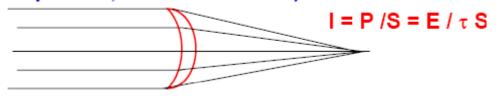


DUE FOTONI INDISTINGUIBILI: STESSA FREQUENZA, DIREZIONE, FASE E POLARIZZAZIONE

In termini semplici possiamo pensare ad una sorta



In pratica una coerenza elevata implica una elevata focalizzabilità del laser (macchia focale molto piccola, intensità elevata)



#### **COERENZA I**

Coerenza nasce da emissione stimolata (e, in genere, proveniente da piccolo volume di mezzo attivo)

Come si può caratterizzare meglio?

The radiation emitted by an extended source S generates a total field amplitude A at the point P which is a superposition of an infinite number of partial waves with the amplitudes  $A_n$  and the phases  $\phi_n$  emitted from the different surface elements dS (Fig.2.21), i.e.,

$$A(P) = \sum A_n(P) e^{i\phi n(P)} = \sum [A_n(0)/r_n^2] e^{i(\phi n_0 + 2\pi r_n/\lambda)}, \qquad (2.89)$$

where  $\phi_{n0}(t) = \omega t + \phi_n(0)$  is the phase of the n<sup>th</sup> partial wave at the surface element dS of the source. The phases  $\phi_n(r_n, t)$  depend on the distances  $r_n$  from the source and on the angular frequency  $\omega$ .

If the phase differences  $\Delta\phi_n=\phi_n(P,t_1)-\phi_n(P,t_2)$  at a given point P between two different times  $t_1$ ,  $t_2$  are nearly the same for all partial waves, the radiation field at P is called temporally coherent. The maximum time intervall  $\Delta t=t_2-t_1$  for which  $\Delta\phi_n$  for all partial waves differ by less than  $\pi$  is termed the coherence time of the radiation source. The path length  $\Delta s_c=c\Delta t$  travelled by the wave during the coherence time  $\Delta t$  is the coherence length.

If a constant time-independent phase difference  $\Delta \phi = \phi(P_1) - \phi(P_2)$  exists for the total amplitudes  $A = A_0 e^{i\phi}$  at two different points  $P_1$ ,  $P_2$  the radiation field is called spatially coherent. All points  $P_m$ ,  $P_n$  which fulfil the condition that for all times t,  $|\phi(P_m,t)-\phi(P_n,t)| < \pi$ , have nearly the same optical path difference from the source. They form the coherence volume.

The superposition of coherent waves results in interference phenomena which, however, can be observed directly only within the coherence volume. The dimensions of this coherence volume depend on the size of the radiation source, on the spectral width of the radiation and on the distance between source and observation point P.

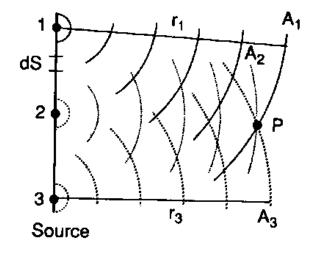


Fig.2.21. The field amplitudes  $A_n$  at a point P in a radiation field as superposition of an infinite number of waves from different surface elements  $dS_i$  of an extended source

Luce coerente può dare luogo a fenomeni di interferenza (nel *volume di coerenza*)

## **COERENZA II**

#### 2.7.1 Temporal Coherence

Consider a point source PS in the focal plane of a lens forming a parallel light beam which is divided by a beam splitter S into two partial beams (Fig. 2.22). They are superimposed in the plane of observation B after reflection from the mirrors  $M_1$ ,  $M_2$ . This arrangement is called a *Michelson interferometer* (Sect.4.2). The two beams with wavelength  $\lambda$  travel different optical path lengths  $SM_1SB$  and  $SM_2SB$ , and their path difference in the plane B is

$$\Delta s = 2(SM_1 - SM_2)$$

The mirror  $M_2$  is mounted on a carriage and can be moved, resulting in a continuous change of  $\Delta s$ . In the plane B, one obtaines maximum intensity when both amplitudes have the same phase, which means  $\Delta s = m\lambda$ , and minimum intensity if  $\Delta s = (2m+1)\lambda/2$ . With increasing  $\Delta s$ , the contrast  $(I_{max}-I_{min})/(I_{max}+I_{min})$  decreases and vanishes if  $\Delta s$  becomes larger than the coherence length  $\Delta s_c$  (Sect.2.7.4). Experiments show that  $\Delta s_c$  is related to the spectral width  $\Delta \omega$  of the incident wave by

$$\Delta s_c \simeq c/\Delta \omega = c/(2\pi\Delta \nu)$$
 (2.90)

This observation may be explained as follows. A wave emitted from a point source with the spectral width  $\Delta\omega$  can be regarded as a superposition of many quasi-monochromatic components with frequencies  $\omega_n$  within the interval  $\Delta\omega$ . The superposition results in wave trains of finite length  $\Delta s_c = c\Delta t = c/\Delta\omega$  because the different components with slightly different frequencies  $\omega_n$  come out of phase during the time interval  $\Delta t$  and interfere destructively causing the total amplitude to decrease (Sect.3.1). If the path difference  $\Delta s$  in the Michelson interferometer becomes larger than  $\Delta s_c$ , the split wave trains no longer overlap in the plane B. The coherence lengths  $\Delta s_c$  of a light source therefore becomes larger with decreasing spectral width  $\Delta\omega$ .

# PS S M

Fig.2.22. Michelson interferometer for measurements of the temporal coherence of radiation from the source S

Coerenza temporale del fascio essenziale per misure di interferometria Ad esempio: misure dimensionali (non invasive) di componenti meccanici con precisione nanometrica

#### Example 2.8

- a) A low-pressure mercury spectral lamp with a spectral filter which only transmits the green line  $\lambda = 546$  nm has, because of the Doppler width  $\Delta\omega_{\rm D} = 4\cdot 10^9$  Hz, a coherence length of  $\Delta s_{\rm c} \simeq 8$  cm.
- b) A single-mode HeNe laser with a bandwidth of  $\Delta \nu = 1$  MHz has a coherence length of about 50 m.



Coerenza richiede monocromaticità!

# **PROFILOMETRIA OTTICA**

Estensione tecniche interferometriche al caso 2D: profilometria ottica (senza contatto)

#### Non-contact profilometers

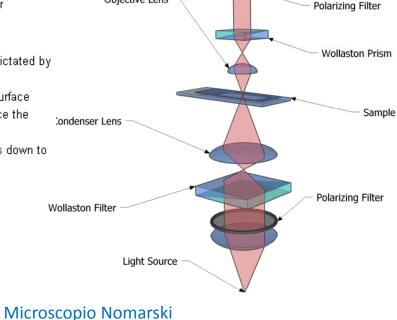
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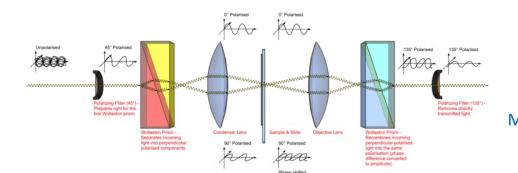
Objective Lens

An optical profilometer is a non-contact method for providing much of the same information as a stylus based profilometer. There are many different techniques which are currently being employed, such as laser triangulation (triangulation sensor), confocal microscopy and digital holography.

#### Advantages of optical profilometers

- Speed: Because the non-contact profilometer does not touch the surface the scan speeds are dictated by the light reflected from the surface and the speed of the acquisition electronics.
- Reliability: optical profilometers do not touch the surface and therefore cannot be damaged by surface wear or careless operators. Many non-contact Profilometers are solid-state which tends to reduce the required maintenance significantly.
- Spot size: The spot size, or lateral resolution, of optical methods ranges from a few micrometres down to sub micrometre.





Due fasci hanno diverso cammino ottico dipendente da posizione  $\rightarrow$  sensibilità fase (essenziale usare fasci coerenti)

Altre tecniche possibili con fasci coerenti: microscopia confocale, ellissometria, etc.

Light Detector

#### **COERENZA III**

#### 2.7.2 Spatial Coherence

The radiation from an extended source LS of size b illuminates two slits S<sub>1</sub> and S<sub>2</sub> in the plane A a distance d apart (Young's double-slit interference experiment, Fig.2.23a). The total amplitude and phase at each of the two slits are obtained by superposition of all partial waves emitted from the different surface elements df of the source, taking into account the different paths  $df-S_1$  and  $df-S_2$ .

The intensity at the point of observation P in the plane B depends on the path difference  $S_1P-S_2P$  and on the phase difference  $\Delta \phi = \phi(S_1)-\phi(S_2)$ of the total field amplitudes in S<sub>1</sub> and S<sub>2</sub>. If the different surface elements df of the source emit independently with random phases (thermal radiation source) the phases of the total amplitudes in  $S_1$  and  $S_2$  will also fluctuate randomly. However, this would not influence the intensity in P as long as these fluctuations occur in S<sub>1</sub> and S<sub>2</sub> synchronously, because then the phase difference  $\Delta\phi$  would remain constant. In this case, the two slits form two coherent sources which generate an interference pattern in the plane B.

For radiation emitted from the central part 0 of the light source this proves to be true since the paths  $0S_1$  and  $0S_2$  are equal and all phase fluctuations in 0 arrive simultaneously in  $S_1$  and  $\bar{S}_2$ . For all other points Q of the source, however, path differences  $\Delta s_Q = QS_1 - QS_2$  exist, which are largest for the edges R of the source. From Fig. 2.23b one can infer for b << r the elation

$$\Delta s_R = R_1 S_2 - R_1 S_1 = R_2 S_1 - R_1 S_1 \simeq b \sin(\theta/2)$$
.

For  $\Delta s_R > \lambda/2$  the phase difference  $\Delta \phi$  of the partial amplitudes in  $S_1$  and  $i_2$  exceeds  $\pi$ . With random emission from the different surface elements df of the source, the time-averaged interference pattern in the plane B will be vashed out. The condition for coherent illumination of  $S_1$  and  $S_2$  from a ight source with the dimension b is therefore

$$\Delta s = b\sin(\theta/2) < \lambda/2.$$

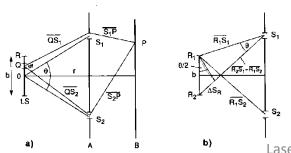


Fig.2.23a.b. Young's double-slit arrangement for measurements of

With  $2\sin(\theta/2) = d/r$ , this condition can be written as

$$bd/r < \lambda$$
. (2.91a)

Extension of this coherence condition to two dimensions yields for a source area  $A_a = b^2$  the following condition for the maximum surface  $A_c =$ d<sup>2</sup> which can be illuminated coherently:

$$b^2 d^2/r^2 \le \lambda^2$$
 (2.91b)

Since  $d\Omega = d^2/r^2$  is the solid angle accepted by the illuminated surface  $A_c =$ d2 this can be formulated as

$$A_{\bullet}d\Omega \le \lambda^2 \ . \tag{2.91c}$$

The source surface  $A_s = b^2$  determines the maximum solid angle  $d\Omega \le$  $\lambda^2/A_a$  inside which the radiation field shows spatial coherence. Equation (2.91c) reveals that radiation from a point source (spherical waves) is spatially coherent within the whole solid angle  $d\Omega = 4\pi$ . The coherence surfaces are spheres with the source in the center. Likewise, a plane wave produced by a point source in the focus of a lens shows spatial coherence over the whole aperture confining the light beam. For given source dimensions, the coherence surface  $A_c = d^2$  increases with the square of the distance from the source. Because of the vast distances to stars, the starlight received by telescopes is spatially coherent across the telescope aperture in spite of the large diameter of the radiation source.

The arguments above may be summarized as follows: The coherence surface S<sub>c</sub>, i.e., that maximum area A<sub>c</sub> which can be coherently illuminated at a distance r from an extended quasi-monochromatic light source with the area A, emitting at a wavelength  $\lambda$  is determined by

$$S_{c} = \lambda^{2} r^{2} / A_{s} . \tag{2.92}$$

Coerenza spaziale: area che può essere illuminata con luce coerente Coerenza spaziale soddisfatta da onda armonica piana monocromatica (fronte d'onda piano infinito!)

#### **COERENZA IV**

#### 2.7.3 Coherence Volume

With the coherence length  $\Delta s_c = c/\Delta \omega$  in the propagation direction of the radiation with the spectral width  $\Delta \omega$  and the coherence surface  $S_c = \lambda^2 r^2/A_a$  the coherence volume  $V_c = S_c \Delta s_c$  becomes

$$V_{c} = \frac{\lambda^{2} r^{2} c}{\Delta \omega A_{s}}.$$
 (2.93)

A unit surface element of a source with the spectral radiance  $L_{\omega}$  [W/m<sup>2</sup>·sterad] emits within the frequency interval  $d\omega = 1$  Hz  $L_{\omega}/\hbar\omega$  photons per second into the unit solid angle 1 sterad.

The mean number  $\bar{n}$  of photons in the spectral range  $\Delta\omega$  within the coherence volume defined by the solid angle  $\Delta\Omega=\lambda^2/A_s$  and the coherence length  $\Delta s_c=c\Delta t_c$  generated by a source with area  $A_s$  is therefore

$$\bar{\mathbf{n}} = (\mathbf{L}_{\omega}/\hbar\omega)\mathbf{A}_{s}\Delta\Omega\Delta\omega\Delta\mathbf{t}_{c} .$$

With  $\Delta\Omega = \lambda^2/A_s$  and  $\Delta t_c \simeq 1/\Delta\omega$  this gives

$$\bar{\mathbf{n}} = (\mathbf{L}_{\omega}/\hbar\omega)\lambda^2 \ . \tag{2.94}$$

#### Example 2.9

For a thermal radiation source, the spectral radiance for linearly polarized light [(2.25) divided by a factor 2] is for  $\cos\phi = 1$  and  $L_{\nu} d\nu = L_{\omega} d\omega$ 

$$L_{\nu} = \frac{h\nu^3/c^2}{e^{h\nu/kT}-1}.$$

The mean number of photons within the coherence volume is then with  $\lambda = c/\nu$ 

$$\bar{n} = \frac{1}{e^{h\nu/kT} - 1}$$
. Sorgente termica (corpo nero)

This is identical to the mean number of photons per mode of the thermal radiation, as derived in Sect. 2.2. Figure 2.5 and Example 2.3 give values of  $\bar{n}$  for different conditions

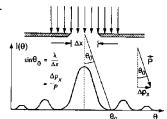


Fig.2.24. The uncertainty principle applied to the diffraction of light by a slit

The mean number  $\bar{n}$  of photons per mode is often called the *degeneracy parameter* of the radiation field. This example shows that the coherence volume is related to the modes of the radiation field. This relation can be also illustrated in the following way:

If we allow the radiation from all modes with the same direction of k to escape through a hole in the cavity wall with the area  $A_g = b^2$ , the wave emitted from  $A_g$  will not be strictly parallel but will have a diffraction-limited divergence angle  $\theta \simeq \lambda/b$  around the direction of k. This means that the radiation is emitted into a solid angle  $d\Omega = \lambda^2/b^2$ . This is the same solid angle (2.91c) which limits the spatial coherence.

The modes with the same direction of k (which we assume to be the z direction) may still differ in  $|\mathbf{k}|$ , i.e., they may have different frequencies  $\omega$ . The coherence length is determined by the spectral width  $\Delta\omega$  of the radiation emitted from  $A_s$ . Since  $|\mathbf{k}| = \omega/c$  the spectral width  $\Delta\omega$  corresponds to an interval  $\Delta k = \Delta\omega/c$  of the k values. This radiation illuminates a minimum "diffraction surface"

$$A_D = r^2 d\Omega = r^2 \lambda^2 / A_g$$

Multiplication with the coherence length  $\Delta s_c = c/\Delta \omega$  yields again the coherence volume  $V_c = A_D c/\Delta \omega = r^2 \lambda^2 c/(\Delta \omega A_s)$  of (2.93). We shall now demonstrate that the coherence volume is identical with the spatial part of the elementary cell in the general phase space.

As is well known from atomic physics, the diffraction of light can be explained by Heisenberg's uncertainty relation. Photons passing through a slit of width  $\Delta x$  have the uncertainty  $\Delta p_x$  of the x component  $p_x$  of their momentum p, given by  $\Delta p_x \Delta x \ge \hbar$  (Fig. 2.24).

Generalized to three dimensions, the uncertainty principle postulates that the simultaneous measurements of momentum and location of a photon has the minimum uncertainty

$$\Delta p_{x} \Delta p_{y} \Delta p_{z} \Delta x \Delta y \Delta z \ge \hbar^{3} = V_{ph} , \qquad (2.95)$$

where  $V_{ph}=\hbar^3$  is the volume of one cell in phase space. Photons within the same cell of the phase space are indistinguishable and can be therefore regarded as identical.

Photons which are emitted from the hole  $A_s = b^2$  within the diffraction angle  $\theta = \lambda/b$  against the surface normal (Fig.2.25), which may point into the z direction, have the minimum uncertainty

$$\Delta p_{x} = \Delta p_{y} = |\mathbf{p}| \lambda/(2\pi \mathbf{b}) = (\hbar \omega/\mathbf{c}) \lambda/(2\pi \mathbf{b}) = (\hbar \omega/\mathbf{c}) d/(2\pi \mathbf{r}), \qquad (2.96)$$

of the momentum components  $p_x$  and  $p_y$  (the last equality follows from (2.91b).

Volumedicoerenza⁄≕iArea c. x Lungh. c (cioè vel./tempō c.)

The uncertainty  $\Delta p_z$  is mainly caused by the spectral width  $\Delta \omega$ . Since  $p = \hbar \omega/c$ , we find

$$\Delta p_{z} = (\hbar/c)\Delta\omega . \tag{2.97}$$

Substituting (2.96,97) into (2.95) we obtain for the spatial part of the phase-space cell

$$\Delta x \Delta y \Delta z = \frac{\lambda^2 r^2 c}{\Delta \omega A_s} = V_c$$
,

which turns out to be identical with the coherence volume defined by (2.93).

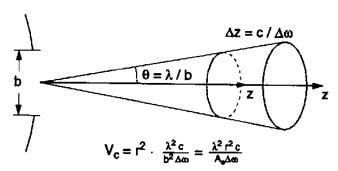


Fig.2.25. Coherence volume and phase space cell

44

Volume di coerenza rappresenta regione in cui i fotoni si comportano allo stesso modo

Rozzamente, volume di coerenza dipende da:

- Area di coerenza ← spazio delle fasi reale
- Lunghezza di coerenza ← tempo coerenza
   ← monocromaticità

Fotoni emessi da piccolo volume di mezzo attivo per emissione spontanea appartengono alle stesse celle dello spazio delle fasci, cioè sono indistinguibili (quantisticamente)

- → Grande volume di coerenza
- → Grande densità di modi fotonici

Nota: luce coerente può essere efficacemente focalizzata (è un time reversal rispetto alla generazione), con il solo limite della diffrazione

#### **BRILLANZA**

#### 1.4.4. Brightness

We define the brightness of a given source of em waves as the power emitted per unit surface area per unit solid angle. To be more precise let dS be the elemental surface area at point O of the source (Fig. 1.7a). The power dP emitted by dS into a solid angle  $d\Omega$  around direction OO' can be written as:

$$dP = B\cos\theta \ dS \ d\Omega \tag{1.4.3}$$

where  $\theta$  is the angle between OO' and the normal  $\mathbf{n}$  to the surface. Note that the factor  $\cos\theta$  occurs because the physically important quantity for emission along the OO' direction is the projection of dS on a plane orthogonal to the OO' direction, i.e.,  $\cos\theta$  dS. The quantity B defined through Eq. (1.4.3) is called the *source brightness* at point O in the direction OO'. This quantity generally depends on polar coordinates  $\theta$  and  $\phi$  of the direction OO' and on point O. When O is a constant, the source is said to be isotropic (or a Lambertian source).

Let us now consider a laser beam of power P, with a circular cross section of diameter D and with a divergence  $\theta$  (Fig. 1.7b). Since  $\theta$  is usually very small, we have  $\cos\theta \cong 1$ . Since the area of the beam is equal to  $\pi D^2/4$  and the emission solid angle is  $\pi \theta^2$ , then, according to Eq. (1.4.3), we obtain the beam brightness as:

$$B = \frac{4P}{(\pi D\theta)^2} \tag{1.4.4}$$

Note that, if the beam is diffraction limited, we have  $\theta=\theta_d$ , and, with the help of Eq. (1.4.1), we obtain from Eq. (1.4.4):

$$\beta : \text{fattore geometrico} \sim 1$$
(1.4.5)

which is the maximum brightness for a beam of power P.

Brightness is the most important parameter of a laser beam and, in general, of any light source. To illustrate this point we first recall that, if we form an image of any light source through a given optical system and if we assume that the object and image are in the same medium (e.g., air), then the following property holds: The brightness of the image is always less than or equal to that of the source, the equality holding when the optical system provides lossless imaging of the light emitted by the source. To illustrate further the importance of

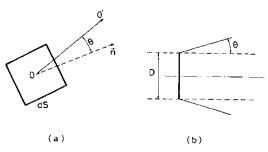


FIG. 1.7. (a) Surface brightness at the point O for a general source of em waves. (b) Beightness of a faser beam  $\frac{1}{2}$   $\frac{1}{2}$  diameter D and divergence  $\theta$ .

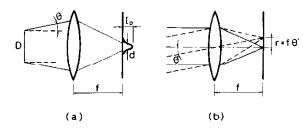


FIG. 1.8. (a) Intensity distribution in the focal plane of a lens for a beam of divergence  $\theta$ . (b) Plane wave decomposition of the beam in (a).

brightness, let us consider the beam in Fig. 1.7b, with divergence equal to  $\theta$ , to be focused by lens of focal length f. We are interested in calculating the peak intensity of the beam in the focal plane of the lens (Fig. 1.8a). To make this calculation we recall that the beam can be decomposed into a continuous set of plane waves with an angular spread of approximately  $\theta$  around the propagation direction. Two such waves, making an angle  $\theta'$ , are indicated by solid and dashed lines, respectively, in Fig. 1.8b. The two beams are each focused on a distinct spot in the focal plane, and, for a small angle  $\theta'$ , the two spots are transversly separated by a distance  $r = f\theta'$ . Since the angular spread of the plane waves that make up the beam in Fig. 1.8a equals the beam divergence  $\theta$ , we conclude that the diameter d of the focal spot in Fig. 1.8a is approximately equal to  $d = 2f\theta$ . For an ideal lossless lens, the overall power in the focal plane equals the power P of the incoming wave. The peak intensity in the focal plane is thus  $I_p = 4P/\pi d^2 = P/\pi (f\theta)^2$ . In terms of beam brightness, according to Eq. (1.4.4), we then have  $I_p = (\pi/4)B(D/f)^2$ . Thus  $I_p$  increases with increasing beam diameter D. The maximum value of  $I_p$  is then attained when D is made equal to the lens diameter D. In this case we obtain

$$I_p = \left(\frac{\pi}{4}\right) (N.A.)^2 B \tag{1.4.6}$$

where  $N.A. = \sin[\tan^{-1}(D_L/f)] \cong (D_L/f)$  is the lens numerical aperture. Equation (1.4.6) then shows that, for a given numerical aperture, the peak intensity in the focal plane of a lens depends only on beam brightness.

A laser beam of even moderate power (e.g., a few milliwatts) has a brightness several graders of magnitude greater than that of the brightest conventional sources (see, e.g., Problem I.7). This is mainly due to the highly directional properties of the laser beam. According to Eq. (1.4.6) this means that the peak intensity produced in the focal plane of a lens can be everal orders of magnitude greater for a laser beam compared to that of a conventional source. Thus the intensity of a focused laser beam can reach very large values, a feature proloited in many applications of lasers.

Es.: HeNe, 1mW, 633nm:  $B^{\sim}10^9$  W/m<sup>2</sup>  $I_p>10^4$  W/cm<sup>2</sup>~3x10<sup>22</sup> fotoni/(s cm<sup>2</sup>) Parte [>>edensità superficiale tipica materia] 7

# **POTENZA ED INTENSITÀ LASER**

Molte applicazioni dei laser dipendono da elevate intensità Oltre a coerenza (direzionalità e possibilità di focalizzare), intensità dipende da carattere amplificatore di mezzo attivo

Potenze *tipiche* di alcuni laser CW (in continua):

-HeNe: 1-50 mW

-Ar<sup>+</sup>: 0.1-10 W -CO<sub>2</sub>: 10 W- kW

-Nd:YAG (e simili): 5-50 W

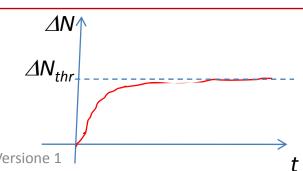
-Diodo: 10 mW – 10 W ("barrette")

# Limitazioni tecnologiche per la potenza:

- Efficienza pompaggio (valori tipici 1-10%);
- Complicati sistemi accessori (raffreddamento, alimentazione, controllo, etc.);
- Densità del mezzo attivo (al massimo idealmente vengono emessi  $n/\tau$  fotoni/(volume secondo)
- Robustezza del mezzo attivo (il mezzo attivo è interessato da potenze paragonabili a quelle di emissione)

# Limitazione fisica per la potenza:

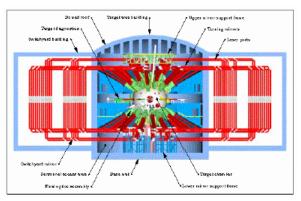
 $-\Delta N \rightarrow \Delta N_{thr}$  in condizioni stazionarie  $\rightarrow$  guadagno tende a un limite



# LASER DI INTENSITÀ STRAORDINARIA

Richiesta di sorgenti laser sempre più intense: applicazioni *ordinarie* (e.g., trattamento materiali) o straordinarie (esempio: fusione inerziale, plasmi densi, etc.)

# Fusione Termonucleare controllata



Nd:vetr 2 MJ 10 ns 200 fasi

 $\lambda = 1.3 \ \mu m \ \tau = 450 \ psec \ E = 1500 \ J$ 



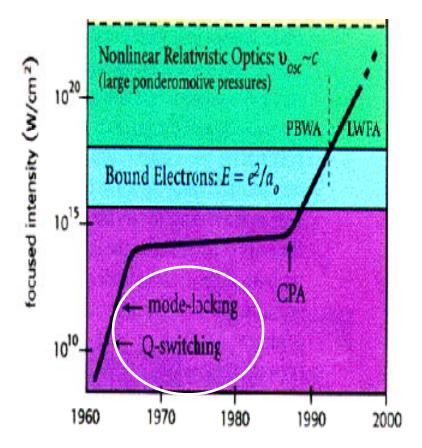


Figure 1. Laser intensity as a function of year, showing the impact of the CPA concept and the different thresholds of physical regimes. The sharp increase in intensity since the advent of CPA is comparable to the sharp increase after the invention of the laser in the 1960's.

Necessarie sorgenti con funzionamento impulsato

#### LASER IMPULSATI

Funzionamento impulsato talvolta è inevitabile per:

- -ragioni tecnologiche (e.g., facilità innesco scarica in miscele gassose, disponibilità lampade flash, etc.)
- -Specifiche pompaggio (e.g., laser ad eccimeri)

Talvolta funzionamento impulsato studiato specificamente per aumentare intensità

Parametro importante per laser impulsati: energia per impulso  $(E = N_{pulse}h v)$ La potenza di picco  $P_{peak}=E/t$  può diventare gigante se t è molto piccolo! La potenza media P=Ef può rimanere ragionevolmente piccola

Es.: laser eccimeri XeCl:, 308 nm, commerciale:

E= 0.5 J, 
$$t = 20$$
 ns,  $f = 100$  Hz  $\rightarrow P_{peak} = 2.5 \times 10^7$  W,  $P = 50$  W (ed  $N_{pulse} \sim 10^{18}$  fotoni)

```
Frequenza di ripetizione CW, 100 MHz, kHz, Hz, single shot Potenza Media P mW \rightarrow W \rightarrow kW Energia per impulso E = P/f pJ \rightarrow mJ \rightarrow J \rightarrow kJ Durata impulso E = P/f pJ \rightarrow mJ \rightarrow J \rightarrow kJ E = P/f pJ \rightarrow mJ \rightarrow J \rightarrow kJ E = P/f pJ \rightarrow mJ \rightarrow J \rightarrow kJ E = P/f pJ \rightarrow mJ \rightarrow J \rightarrow kJ E = P/f E = P
```

# Q-SWITCHING I

#### 8.4. Q-SWITCHING

In Chap, 7 we saw that, under cw operation, the population inversion is fixed at its threshold value when oscillation starts. Even under the pulsed operating conditions considered in Sect. 8.2, the population inversion is seen to exceed the threshold value by only a relatively small amount (see Fig. 8.1) due to the onset of stimulated emission. Suppose now that a shutter is introduced into the laser cavity. In the shutter is closed, laser action is prevented, so the value of the population inversion may far exceed the threshold population holding when the shutter is absent. If the shutter is now opened suddenly, the laser will exhibit a gain that greatly exceeds losses; stored energy may then be released in the form of a short and intense light pulse. (8) Since this operation involves switching the eavity Q-factor from a low to a high value, the technique is usually called Q-switching. This technique allows one to generate laser pulses with a duration comparable to the photon decay time (i.e., from a few nanoseconds to a few tens of nanoseconds) and high-peak power (in the megawatt range).

#### 8.4.1. Dynamics of the O-Switching Process

To describe the Q-switching dynamic behavior, we assume that a step pump pulse is applied to the laser starting at time t = 0, i.e.,  $R_p(t) = 0$  for t < 0 and  $R_n(t) = R_n = \text{constant}$ for  $0 < t < t_n$ ; meanwhile the shutter is closed (Fig. 8.3a). For  $0 < t < t_n$ , the time behavior of the population inversion can be calculated from Eq. (7.2.16a), for a four-level laser, or

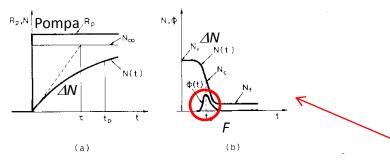


FIG. 8.3. Sequence of events in a Q-switched laser: (a) Idealized time behavior of the pump rate,  $R_n$ , and of the population inversion, N, before Q-switching. (b) Time behavior of population inversion, N, and photon number,  $\phi$ . after O-switching (fast switching case.)

Q-switching: la cavità è "temporizzata" Maggiore energia incameratain mezzo attivo from Eq. (7.2.24a), for a quasi-three-level laser, with  $\phi$  set to zero. For instance, for a fourlevel laser, we obtain

$$N(t) = N_{\infty} [1 - \exp(-t/\tau)]$$
 (8.4.1)

where the asymptotic value  $N_{\infty}$  is given by:

$$N_{\infty} = R_n \tau \tag{8.4.2}$$

as we readily obtain from Eq. (7.2.16a) by setting dN/dt = 0. The time behavior of N(t) is also shown in Fig. 8.3a. From Eq. (8.4.1) and Fig. 8.3a we see that the duration  $t_n$  of the pump pulse ideally should be comparable to, or shorter than, the upper state lifetime r. In fact, for  $t_n \gg \tau$ , N(t) does not undergo any further appreciable increase and the pump power, rather than being accumulated as inversion energy, would be wasted through spontaneous decay. From Eq. (8.4.2) we also see that, to achieve a sufficiently large inversion, a long lifetime  $\tau$  is required. Thus Q-switching can be used, effectively, with electric-dipoleforbidden laser trensitions, where τ generally falls in the millisecond range. This is the case of most solid-state lasers e.g., Nd, Yb, Er, Ho in different host materials; Cr-doped materials, such as alexandrite, Cr:LiSAF, and ruby) and some gas lasers (e.g., CO2 or iodine). On the other hand, for semiconductor lasers, dye lasers, and a number of important gas lasers (e.g., He-Ne, Ar, Excimers), the laser transition is electric-dipole allowed and the lifetime is on the order of a few to a few tens of nanoseconds. In this case, with the usual values for pump rates  $R_p$  available, the achievable inversion  $N_{\infty}$  is too low to be of interest for O-switching.

We now assume that the shutter is suddenly opened at time  $t = t_p$ , so that cavity loss y(t) is switched from a very high value, corresponding to a closed shutter, to the value y for the same cavity with the shutter open (fast switching) We now take the time origin at the instant when switching occurs (Fig. 8.3b). The time behavior of the population inversion. N(t) and the number of photons  $\phi(t)$  can then be obtained from the rate equations with the simplifying assumption that, during the short time of the Q-switching process, the effect of the decay term  $N/\tau$  can be neglected. The qualitative behavior of N(t) and  $\phi(t)$  can then be depicted as in Fig. 8.3b. The population inversion starts from the initial value  $N_i$ , which can be obtained from Eq. (8.4.1) for  $t = t_P$ , then remains constant for some time, and finally begins to be depleted when the cavity photon number reaches a sufficiently high value. When N(t) eventually falls to the threshold inversion  $N_c$ , the photon number reaches its peak value, as discussed earlier for the case of relaxation oscillations in Sect. 8.2. From this time on, the laser exhibits net loss rather than net gain; as a consequence, the photon number decreases to zero. During the same time the population inversion decreases to a final value  $N_6$  which is left in the active medium; its value is established by the dynamics of the Qswitching process (see Sect. 8.4.4). Note that the time scales in Figs. 8.3a-b are very different; in fact, the time scale in Fig. 8.3a is established by the value of the upper state lifetime and thus corresponds to the microsecond range (usually, 100 µs-1 ms). The time scale in Fig. 8.3b, on the other hand, turns out to be of the order of the cavity photon decay time (see Sect. 8.4.4) and hence falls in the nanosecond range (usually, 5-50 ns).

So far we have considered the dynamic behavior corresponding to fast switching, where the switching of cavity loss is treated as instantaneous. In practice, fast switching requires

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# **Q-SWITCHING II**

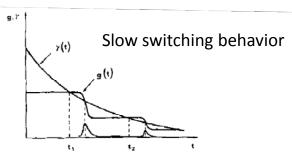


FIG. 8.4. Sequence of events in the slow switching case demonstrating the occurrence of multiple pulses. In the igure,  $g(t) = \sigma N(t) l$ , where l is the length of the active medium, represents the laser gain.

their peak value (several photon decay times, i.e., typically from a few tens to a few hundreds of a nanosecond). In the case of slow switching, the dynamic behavior is somewhat more complicated and multiple pulses may result. Figure 8.4 depicts this behavior, where cavity loss  $\gamma(t)$  is assumed to decay from its initially high value to a final value in a relatively long time. The same figure also shows the corresponding time behavior of the single-pass gain  $g(t) = \sigma Nl$  and the cavity photon number  $\phi(t)$ . The first pulse starts at time  $t_1$  when the decreasing loss  $\gamma(t)$  equals the instantaneous gain g(t). The pulse then reaches its peak value when the gain, owing to its decrease due to saturation, equals the loss. After this first pulse, the gain is driven below the loss, so further oscillation cannot occur until the switch opens further, thus decreasing the loss below the gain. A second pulse can then be produced (occurring at time  $t_2$  in the figure) whose peak again occurs when gain saturation makes the gain equal to loss.

#### 8.4.2. Q-Switching Methods

Several methods have been developed to achieve switching of the cavity Q; in this section we limit ourselves to discussing the most commonly used, namely: <sup>(9)</sup> (1) Electro-optical shutters. (2) Rotating prisms. (3) Acoustooptical switches. (4) Saturable absorbers. These devices are generally grouped into two categories, active and passive Q-switches. In an active Q-switching device, some external active operation must be applied to this device (e.g., a change of the voltage applied to the electrooptical shutter) to produce Q-switching. In a passive Q-switch, the switching operation is automatically produced by the optical nonlinearity of the element used (e.g., a saturable absorber).

#### 8.4.2.1. Electrooptical Q-Switching

These devices use a cell exploiting an electrooptical effect, usually the Pockels effect, to induce Q-switching. A cell based on the Pockels effect (Pockels cell) consists of a suitable nonlinear crystal, such as KD\*P or lithium niobate for the visible-to-near-infrared region or cadmium telluride for the middle-infrared, in which an applied de voltage induces a change

in the crystal's refractive indices. This induced birefringence turns out to be proportional to the applied voltage. Figure 8.5a shows a Q-switched laser using a suitable combination of a polarizer and a Pockels cell. The Pockels cell is oriented and biased so that the x- and y-axes of the induced birefringence lie in the plane orthogonal to the resonator axis. The polarizer axis then makes a 45° angle to the birefringence axes.

Consider now a laser beam propagating from the active medium toward the polarizer-Pockels cell combination with polarization parallel to the polarizer axis. Ideally this beam is totally transmitted by the polarizer and then incident on the Pockels cell. The *E*-field of the incoming wave is at  $45^{\circ}$  to the birefringence *x*- and *y*-axes of the Pockels cell and it can be resolved into components  $E_x$  and  $E_y$  (Fig. 8.5b) with their oscillations in phase. After passing through the Pockels cell, these two components have experienced different phase shifts, giving rise to the phase difference:

# Sfasamento (ritardo) tra componenti $E^{3}$

where  $k = 2\pi/\lambda$ ,  $\Delta n = n_x - n_y$  is the value of the induced birefringence, and L' is the crystal length. If the voltage applied to the Pockels cell is such that  $\Delta \varphi = \pi/2$ , then the two field components leaving the Pockels cell differ in phase by  $\pi/2$ . This means that when  $E_x$  is maximum,  $E_y$  is zero and vice versa; i.e., the wave is circularly polarized (Fig. 8.5c). After reflection at the mirror, the wave passes once more through the Pockels cell, so its x- and y-components acquire an additional  $\Delta \varphi = \pi/2$  phase difference. The total phase difference then becomes  $\pi$ , so that, when, e.g.,  $E_x$  is at its maximum (positive) value,  $E_y$  is at its maximum (negative) value, as shown in Fig. 8.5d. As a result, the overall field E is again linearly polarized but with a polarization axis at 90° to that of the original wave in Fig. 8.5b. This beam is therefore not transmitted by the polarizer, but instead it is reflected out of the cavity (see Fig. 8.5a). This condition corresponds to the Q-switch being closed. The switch is then opened by removing the bias voltage to the Pockels cell. In this case the induced

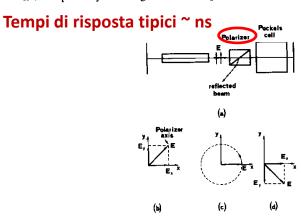
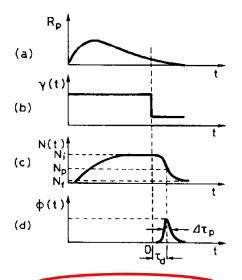


FIG. 8.5. (a) Possible polarizer-Pockels-cell combination for Q-switching. Figures (b), (c), and (d) show the E-field components along the birefringence axes of the Pockels cell in a plane orthogonal to the resonator axis.

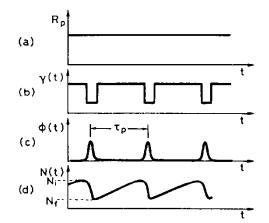
Pockel effect: switch rapido della polarizzazione attraverso birifrangenza (sfasamento tra componenti del campo)

# Q-SWITCHING III



falls in the millisecond range, while the time scale for events when t>0 falls in the nanosecond range. Q-switched lasers with a pulsed pump can obviously be operated repetitively; the typical repetition rates range from a few to a few tens of Hz. (2) Continuously pumped, repetitively Q-switched operation (Fig. 8.10), where a cw pump  $R_p$  is applied to the laser (Fig. 8.10a) and cavity losses are periodically switched from a high to a low value (Fig. 8.10b). Laser output then consists of a continuous train of Q-switched pulses (Fig. 8.10c). During each pulse, inversion falls from its initial value  $N_i$  (before Q-switching) to a final value  $N_f$  (after the Q-switched pulse; see Fig. 8.10d). The population inversion is then restored to its initial value  $N_i$  by the pumping process before the next Q-switching event. Since the time taken to restore the inversion is roughly equal to the upper-state

FIG. 8.9. Development of a Q-switched laser pulse in pulsed operation. The figure shows the time behavior of: (a) the pump rate  $R_p$ ; (b) the resonator loss  $\gamma$ ; (c) the population inversion N; (d) the number of photons  $\phi$ .



Q-switching applicabile in condizioni di pompa impulsata (più frequente) o pompa CW

# Esempi tipici:

-pompa impulsata Nd:YAG,  $E^{\sim}$  0.1 – 1 J,  $t^{\sim}$ 10ps –10ns

-pompa CW: Ar<sup>+</sup>,  $E \sim 10 - 100$  mJ,  $t\sim 1-100$ ns

FIG. 8.10. Development of Q-switched laser pulses in a coefficiently Q-switched, cw pumped laser. The figure shows the time behavior of: (a) the pump rate  $R_p$ ; (b) the resonator losses y; (c) the number of photons  $\phi$ ; (d) the population inversion N.

#### **MODE-LOCKING I**

#### 8.6. MODE LOCKING

Let us now consider a laser oscillating in large number of longitudinal modes Under ordinary circumstances, phases of these modes have random values, and, for cw oscillation beam, intensity shows random time behavior. Figure 8.15 shows the time behavior of the square of the electric field amplitude  $|A(t)|^2$  of the output beam for N=51 oscillating modes, each with the same amplitude  $E_0$ , and evenly separated in frequency by the frequency difference  $\Delta v$  between consecutive longitudinal modes. The output beam is seen to consist of a random sequence of light pulses. Despite this randomness, since these pulses arise from the sum of N trequency components evenly spaced in frequency, the pulse waveform in Fig. 8.15 has the following features which are characteristics of a Fourier series: (1) The waveform is periodic with a period  $t_0 = 1/\Delta v$ . (2) Each light pulse of the random waveform has a duration  $\Delta \tau_p$  roughly equal to  $1/\Delta v_L$ , where  $\Delta v_L = N\Delta v$  is the total oscillating bandwidth. Thus, for lasers with relatively large gain bandwidths, such as solidstate, dye, or semiconductor lasers,  $\Delta v_L$  may be comparable to this bandwidth; hence short noise pulses with durations of picoseconds or less can be produced. Note that, since the response time of a conventional photodetector is usually much longer than a few picoseconds, we do not resolve this complex time behavior in the detected output of a random-phase, multimode laser; instead its average value is monitored. This value is the sum of powers in the modes; hence is proportional to  $NE_0^2$ 

Suppose now that the oscillating modes, while still having equal or comparable amplitudes, are somehow made to oscillate with some definite relation between their phases. Such a laser is referred to as mode locked, and the process by which modes are made to adopt a definite phase relation is referred to as mode locking. (15) Mode-locked lasers are considered at some length in the following sections.

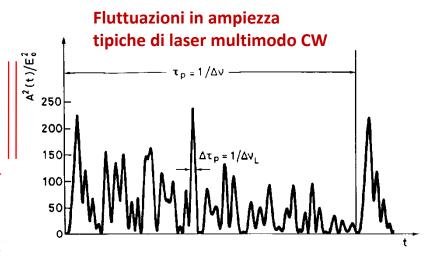


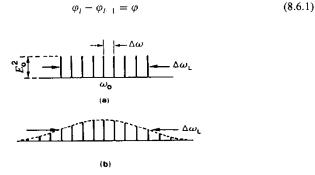
FIG. 8.15. Example of time behavior of the squared amplitude of the total electric field,  $|A(t)|^2$ , for the case of 51 oscillating modes, all with the same amplitude  $E_0$  and with random phases.

Laser multimodo ordinario (CW) con larga forma di riga di guadagno: fotoni nei vari modi La fase dei vari modi è random  $\rightarrow$  fluttuazioni in ampiezza Durata di ogni impulso di fluttuazione  $\sim 1/\Delta v_{laser}$  (cioè inverso di larghezza di guadagno)

#### **MODE-LOCKING II**

#### 8.6.1. Frequency-Domain Description

We first describe mode-locking in the frequency domain and consider, as a first example, the case of 2n + 1 longitudinal modes oscillating with the same amplitude  $E_0$  (Fig. 8.16a). We assume that phases  $\varphi_i$  of the modes in the output beam to be locked according to the relation



*FIG. 8.16.* Mode amplitudes (represented by vertical lines) versus frequency for a mode-locked laser. (a) Uniform amplitude distribution, and (b) Gaussian amplitude distribution, over a bandwidth (FWHM)  $\Delta\omega_L$ .

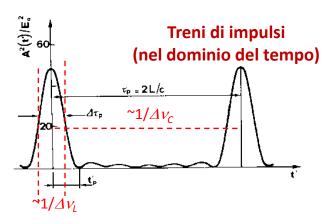


FIG. 8.17. Time behavior of the squared amplitude of the electric field for the case of seven oscillating modes with locked phases and equal amplitudes,  $E_0$ .

La presenza di molti modi di cavità (ognuno a frequenze diverse) produce impulsi nel dominio temporal

wher  $\varphi$  is a constant. The total electric field E(t) of the em wave at any given point in the output beam can be written as:

$$E(t) = \sum_{-n}^{+n} {}_{l}E_{0} \exp\{j\{(\omega_{0} + l\Delta\omega)t + l\varphi\}\}$$
(8.6.2)

where  $\omega_0$  is the frequency of the central mode,  $\Delta\omega$  is the frequency difference between two consecutive modes, and the value of the phase for the central mode has, for simplicity, been taken as zero. According to Eq. (8.6.2), the total electric field of the wave can be written as

$$E(t) = A(t) \exp(j\omega_0 t)$$
 (8.6.3)

where

#### Analisi di Fourier

$$A(t) = \sum_{n=1}^{n} JE_0 \exp[jl(\Delta\omega t + \varphi)]$$
 (8.6.4)

Equation (8.6.3) shows that E(t) can be represented in terms of a sinusoidal carrier wave, at the center mode frequency  $\omega_0$ , whose amplitude A(t) is time-dependent.

To calculate the time behavior of A(t), we now change to a new time reference t' such that  $\Delta \omega t' = \Delta \omega t + \varphi$ . In terms of the new variable t', Eq. (8.6.4) can be transformed into:

$$A(t') = \sum_{-n}^{+n} {}_{t}E_{0} \exp jt(\Delta\omega t')$$
(8.6.5)

The sum on the right-hand side is easily recognized as a geometric progression with a ratio  $\exp j(\Delta \omega t')$  between consecutive terms. This progression is then easily summed to obtain

$$A(t') = E_0 \frac{\sin[(2n+1)\Delta\omega t'/2]}{\sin(\Delta\omega t'/2)}$$
 Funzione<sub>8</sub>di<sub>6</sub>)
"diffrazione"

To understand the physical significance of Eq. (8.6.6), Fig. 8.17 shows the quantity  $A^2(t')/E_0^2$ ,  $A^2(t')$  being proportional to beam intensity, versus time t', for 2n+1=7 oscillating modes. As a result of the phase-locking condition (8.6.1), oscillating modes are seen to interfere so as to produce a train of evenly spaced light pulses. Pulse maxima occur when the denominator in Eq. (8.6.6) vanishes. In the new time reference t', the first maximum occurs for t'=0. Note that, at this time, the numerator in Eq. (8.6.6) also vanishes. Making the approximation  $\sin \alpha \cong \alpha$ , which holds for small values of  $\alpha$ , we readily see from Eq. (8.6.6) that  $A^2(0) = (2n+1)^2 E_0^2$ . The next pulse occurs when the denominator in Eq. (8.6.6) again vanishes; this happens at time t' such that  $(\Delta \omega t'/2) = \pi$ . Two successive pulses are therefore separated by a time:

$$\tau_p = \frac{2\pi}{\Delta\omega} = \frac{1}{\Delta v}$$
 Separatem

# Separazione temporale tra impulsi

where  $\Delta v$  is the frequency separation between two consecutive modes. For t' > 0, the first produce impulsi nel dominio temporale (8.6.6) again vanishes. This

#### **MODE-LOCKING III**

occurs at time  $t_p'$  such that  $[(2n+1)\Delta\omega t_p'/2] = \pi$ . Since the width  $\Delta\tau_p$  (FWHM) of  $A^2(t')$ , i.e., of each laser pulse, is approximately equal to  $t_p'$ , we have

$$\Delta t_p \cong \frac{2\pi}{(2n+1)\Delta\omega} = \frac{1}{\Delta v_L}$$
 Durata dell'impulso

where  $\Delta v_L = (2n + 1)\Delta\omega/2\pi$  is the total laser bandwidth (see Fig. 8.16a).

The mode-locking behavior in Fig. 8.17 can be readily understood if we represent field components in Eq. (8.6.5) by vectors in the complex plane. The *l*th amplitude component thus corresponds to a complex vector of amplitude  $E_0$  rotating at the angular velocity  $l\Delta\omega$ . At time t'=0 these vectors have zero phase [see Eq. (8.6.5)] and, accordingly, they lie in the same direction, which we assume to be the horizontal direction in Fig. 8.18. The total field in this case is  $(2n+1)E_0$ . For t'>0, the vector corresponding to the central mode remains fixed; vectors for modes where t>0, i.e., with  $\omega>\omega_0$ , rotate in one direction (e.g., counterclockwise), while vectors for modes where  $\omega<\omega_0$  rotate in the opposite (clockwise) sense. Thus, in the case of, e.g., five modes, the situation at some later time t' will be as indicated in Fig. 8.18a. If now time t' is such that mode 1 has made a counterclockwise

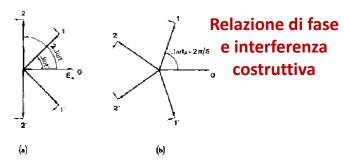


FIG. 8.18. Representation of the cavity mode amplitudes in the complex plane for the case of five modes. (a) shows the situation at a general time t' > 0, while (b) depicts the time instant at which the sum of the five mode amplitudes

rotation of  $2\pi$  (which occurs when  $\Delta\omega t'=2\pi$ ), mode -1 will also have rotated (clockwise) by  $2\pi$ , while modes 2 and -2 will have rotated by  $4\pi$ . Therefore all these vectors are again aligned with the vector at frequency  $\omega_0$  and total field amplitude is again  $(2n+1)E_0$ . Thus the time interval  $\tau_p$  between two consecutive pulses must be such that  $\Delta\omega\tau_p=2\pi$ , as shown by Eq. (8.6.7). In this picture, the time  $t_p'$  at which A(t') vanishes (see Fig. 8.17) corresponds to the situation where all vectors are evenly spaced around the  $2\pi$  angle (Fig. 8.18b). To achieve this condition, mode 1 must have rotated only by  $2\pi/5$  or, more generally for (2n+1) modes, by  $2\pi/(2n+1)$ . The time duration  $t_p'$  and hence the pulse duration  $\Delta\tau_p$  are thus given by Eq. (8.6.8).

Before proceeding we point out here some peculiar properties of mode-locked lasers. We first recall that, under the mode-locking condition given by Eq. (8.6.1), the output beam consists of a train of mode-locked pulses; the duration of each pulse  $\Delta \tau_p$  is about equal to the inverse of the oscillating bandwidth  $\Delta v_L$ . This result is due to a general property of a Fourier series. Since  $\Delta v_L$  can be of the order of the width of the gain line  $\Delta v_0$  very short pulses (down to a few picoseconds) can be expected to result from mode-locking in solid state or semiconductor lasers. For dye or tunable solid-state lasers, the gain linewidth can be at least a factor 100 times larger, so that much shorter pulse widths are possible and indeed have been obtained (e.g.,  $\sim 25$  fs for rhodamine 6G dye laser and  $\stackrel{\checkmark}{\sim} 7$  fs for Ti:sapphire laser) In the case of gas lasers the gain linewidth is much narrower (up to a few GHz) so relatively long pulses are generated (to  $\sim 100$  ps). Note also that the peak power of the pulse is proportional to  $(2n+1)^2 E_0^2$ , whereas, for modes with random phases, average power is simply the sum of powers in the modes and hence proportional to  $(2n+1)E_0^2$ . Therefore, for the same number of oscillating modes and for the same field amplitudes  $E_0$ , the ratio between the peak-pulse power in the mode-locked case and the average power in the nonmode-locked case is equal to the number, (2n + 1), of oscillating modes, which for solidstate or liquid lasers, can be very high  $(10^3-10^4)$ . Mode-locking is thus useful not only for producing pulses of very short duration but also for producing high peak powers.

So far we have restricted our considerations to the unrealistic case of an equalamplitude mode spectrum (Fig. 8.16a). The spectral envelope is generally expected to have a bell shape, however, and, as a simple example, we consider a Gaussian shape (Fig. 8.16b). We can therefore write the amplitude  $E_l$  of the lth mode as:

$$E_I^2 = E_0^2 \exp[-(2l\Delta\omega/\Delta\omega_I)^2 \ln 2]$$
 (8.6.9)

where  $\Delta\omega_L$  represents the bandwidth (FWHM) of the spectral intensity. If we assume that phases are locked according to Eq. (8.6.1) and the phase of the central mode is zero, we find that E(t) can be expressed as in Eq. (8.6.3), where the amplitude A(t'), in the time reference t', is given by:

$$A(t') = \sum_{-\infty}^{\infty} {}_{l}E_{l} \exp j(l\Delta \omega t')$$
 (8.6.10)

If the sum is approximated by an integral [i.e.,  $A(t) \cong \int E_t \exp j(t\Delta \omega t) dt$ ], the field amplitude A(t) is seen to be proportional to the Fourier transform of the spectral amplitude  $E_t$ . We then find that  $A^2(t)$ , i.e., the pulse intensity, is a Gaussian function of time, which can be written as

$$A^{2}(t) \propto \exp[-(2t/\Lambda \tau_{n})^{2} \ln 2]$$
 (8.6.11)

#### Ti:Sa LASER

#### Laser con metalli di transizione (in cristalli)

La debole schermatura degli elettroni 3d negli ioni dei metalli di transizione porta a forti interazioni con i ligandi e può, quindi, dar luogo a bande molto larghe, con conseguente possibilità di accordabilità in frequenza molto ampia e generazione di impulsi ultra brevi. Esempi sono elencati in Tabella 3.3.

Laser	Crystal	Wavelength [nm]
Ruby	Cr³+:Al <sub>2</sub> O <sub>3</sub>	694.4 692.9
Alexandrite	Cr3+:BeAl <sub>2</sub> O <sub>4</sub>	700 - 800
Titanium-sapphire	Ti <sup>3+</sup> :Al <sub>2</sub> O <sub>3</sub>	660-1180
Forsterite	Cr3+:Mg <sub>2</sub> SiO <sub>4</sub>	1167-1345
Nickel-Magnesium	Ni:MgF <sub>2</sub>	1610-1730
Cobalt-Magnesium	Co:MgF2	1650-2010

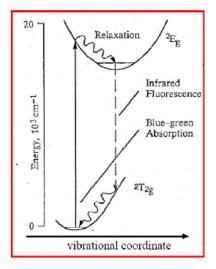
Tabella 3.3. Alcuni laser con metalli di transizione e loro lunghezze d'onda di emissione

#### Ti: Zaffiro (Ti: Al<sub>2</sub>O<sub>3</sub>)

Il cristallo è drogato allo 0.1% con Titanio, il cui ione trivalente sostituisce quello dello Alluminio. L'effetto laser è stato scoperto nel 1982, ma i primi dispositivi sono stati resi commerciali solo nel 1988. Lavorano nel vicino infrarosso e tendono a sostituire i laser a coloranti rispetto ai quali mostrano maggiore stabilità, inferiore rumore e ampiezza di riga di circa 1kHz.

Laser a Ti:Sa (pompaggio simile a Nd:YAG et al.) ha enorme intervallo di guadagno → Impulsi ultracorti facilmente ottenibili!

Pompaggio ottico, spesso con laser Ar<sup>+</sup> o diodo duplicato



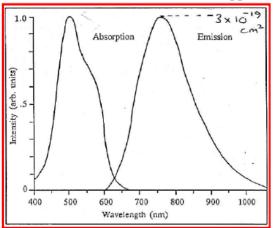
#### Ti:sapphire laser I

- •4-level laser
- Rapid vibronic relaxation in both
- upper & lower bands •Stokes shift between emission &
- •Upper laser level lifetime, 3µs.

absorption profiles

•Stimulated emission cross-section 3x10<sup>-23</sup> m<sup>2</sup>

#### Ti:sapphire laser II



Absorption & Emission Spectra

#### METODI DI MODE-LOCKING

#### Active mode-locking

The most common active mode-locking technique places a standing wave acousto-optic modulator into the laser cavity. When driven with an electrical signal, this produces a sinusoidal amplitude modulation of the light in the cavity. Considering this in the frequency domain, if a mode has optical frequency v, and is amplitude-modulated at a frequency f, the resulting signal has sidebands at optical frequencies v-f and v+f. If the modulator is driven at the same frequency as the cavity-mode spacing  $\Delta v$ , then these sidebands correspond to the two cavity modes adjacent to the original mode. Since the sidebands are driven in-phase, the central mode and the adjacent modes will be phase-locked together. Further operation of the modulator on the sidebands produces phase-locking of the v-2f and v+2f modes, and so on until all modes in the gain bandwidth are locked. As said above, typical lasers are multi-mode and not seeded by a root mode. So multiple modes need to work out which phase to use. In a passive cavity with this locking applied there is no way to dump the entropy given by the original independent phases. This locking is better described as a coupling, leading to a complicated behavior and not clean pulses. Only because of the dissipative nature of the amplitude modulation the coupling is also dissipative, phase modulation would not work.

This process can also be considered in the time domain. The amplitude modulator acts as a weak *shutter* to the light bouncing between the mirrors of the cavity, attenuating the light when it is "closed", and letting it through when it is "open". If the modulation rate *f* is synchronised to the cavity round-trip time \(\tau\_t\), then a single pulse of light will bounce back and forth in the cavity. The actual strength of the modulation does not have to be large; a modulator that attenuates 1% of the light when "closed" will mode-lock a laser, since the same part of the light is repeatedly attenuated as it traverses the cavity.

Related to this amplitude modulation (AM) active mode-locking is frequency modulation (FM) mode-locking, which uses a modulator device based on the electro-optic effect. This device, when placed in a laser cavity and driven with an electrical signal, induces a small, sinusoidally varying frequency shift in the light passing through it. If the frequency of modulation is matched to the round-trip time of the cavity, then some light in the cavity sees repeated up-shifts in frequency, and some repeated down-shifts. After many repetitions, the up-shifted and down-shifted light is swept out of the gain bandwidth of the laser. The only light which is unaffected is that which passes through the modulator when the induced frequency shift is zero, which forms a narrow pulse of light.

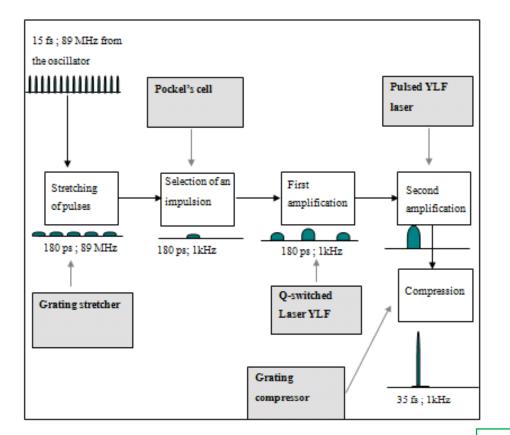
The third method of active mode-locking is synchronous mode-locking, or synchronous pumping. In this, the pump source (energy source) for the laser is itself modulated, effectively turning the laser on and off to produce pulses. Typically, the pump source is itself another mode-locked laser. This technique requires accurately matching the cavity lengths of the pump laser and the driven laser.

Modulatore acusto-ottico (AOM): Cristallo che supporta un'onda acustica (tipicamente 10-200 MHz) Diffrazione di Bragg modulata Uscita: portante modulata in frequenza

Modulatore elettro-ottico (EOM): Idem ,ma onda generata da campo elettrico oscillante

Mode-locking si ottiene (in genere) introducendo sidebands nei modi ottici della cavità Queste sidebands sono modulate (AM o FM) in fase tra loro

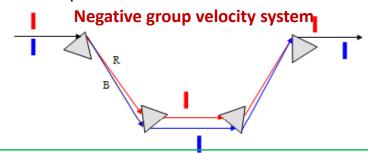
## LASER fs REALISTICI



In genere l'oscillatore è seguito da stadi di amplificazione (per emissione stimolata)

Per aumentare l'efficienza di amplificazione (con pompaggio ottico da altri laser) generalmente gli impulsi si allungano e poi si ricomprimono

Il controllo della durata dell'impulso si fa con ottica dispersiva



# Performance tipica:

- Impulsi da decine di fs
- Frequenze di ripetizione ~ kHz MHz
- Energia impulso ~ 1 − 10 mJ
- Lunghezza d'onda ~ 700 800 nm

# Uso prevalente:

- spettroscopia di sistemi molecolari (eccitazione diretta della dinamica molecolare)
- trattamento materiali (per evitare formazione di plasma)

Nota: per  $t \sim$  fs principio di indeterminazione stabilisce  $\Delta v \sim v$ Laser al a. 2007/08 - Parte Sorgenti (coerenti?) di luce bianca... 29

## **MODE-LOCKING PASSIVO IN FIBRA**

#### 1.5-µm Femtosecond Erbium Fiber Lasers

Erbium-doped fibers, as otherwise used mainly for erbium-doped fiber amplifiers, exhibit a broad gain bandwidth, with a maximum either at 1535nm or at some longer wavelength such as 1550nm – depending on the composition of the fiber core and on the inversion level, which itself is determined by fiber length, doping concentration and resonator losses.

A particularly simple type of erbium-doped fiber laser [4] is shown in Figure 1. The linear laser resonator is terminated by a semiconductor saturable absorber mirror (SESAM) as a passive mode locker on the left-hand side and a bare fiber end (with roughly 4% Fresnel reflection) on the right-hand side. The erbium-doped fiber is pumped with a low-power laser diode, the output of which is introduced into the resonator with a dichroic fiber coupler. The fiber length determines the pulse repetition

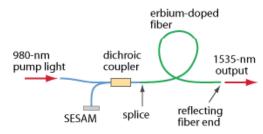


Figure 1: Simple erbium-doped femtosecond fiber laser.

rate, and the pulse duration of e.g. some hundred femtoseconds is determined by the interplay of dispersion, nonlinearity and the gain.

Shorter pulses can be obtained from more sophisticated resonators. An example is the "figure-of-eight" laser setup [3] as shown in Figure 2. The ring on the right-hand side is a nonlinear amplifying loop mirror. Light coming from the main resonator (the left ring) is split into counterpropagating components in the loop mirror. As the light propagating in clock-wise direction first passes a long nonlinear fiber with low power and is then amplified in the erbium-doped fiber, whereas light propagating in the other direction is amplified first, the nonlinear phase shift is larger for the

emitted at the lower left port.

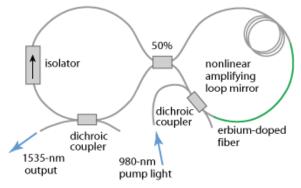


Figure 2: Figure-of-eight laser setup, with a main resonator on the left-hand side an a nonlinear amplifying loop mirror as the mode-locking element.

latter component. If the difference in nonlinear phase shifts is  $\pi$  (the ideal case), the two components will interfere in such a way at the coupler in the middle that all the light is sent towards the bottom of the main resonator; light sent in the other direction will be eliminated by the isolator. The round-trip gain is thus very small for low powers, but much larger in a certain range of powers (ideally arranged to be near the peak power of the pulses). Effectively this setup acts like the combination of some laser gain with a saturable absorber, favoring the peak of a circulating pulse against the low-power background light. This artificial saturable absorber generates a single pulse circulating in the resonator and thus a pulse train.

#### **Fiber gratings**

core	refractive index grating	
cladding		
air		

Figure 1: Schematic structure of a fiber Bragg grating (FBG). The fiber core has a periodically varying refractive index over some length. The drawing is not to scale; typical dimensions are 125µm cladding diameter and 8µm core diameter; periods of the refractive index gratings vary in the range of hundreds of nanometers or (for long-period gratings) hundreds of micrometers.

e refractive index perturbation leads to the reflection of light (propagating along the fiber) in a narrow range of wavelengths, for which a *Bragg condition* is satisfied (→ *Bragg mirrors*):

$$\frac{2\pi}{\Lambda} = 2 \cdot \frac{2\pi n_{\text{eff}}}{\lambda} \implies \lambda = 2n_{\text{eff}} \Lambda$$

where  $\Lambda$  is the grating period,  $\lambda$  is the vacuum wavelength, and  $n_{\rm eff}$  is the effective refractive index of light in the fiber.

Sistemi miniaturizzati basati su fibra

Mode-locking tramite battimento fra diverse cavità (anelli di fibra)

Produzione impulsi ultrabrevi per TLC

# **CONCLUSIONI**

Le proprietà della luce laser sono ben interpretate sulla base del comportamento di:

- emissione stimolata
- guadagno del mezzo attivo (pompato)
- cavità ottica risonante

Esistono tecniche in grado di migliorare alcune caratteristiche della luce, in particolare quelle di larghezza di riga (monocromaticità) e coerenza spaziale

Tecniche si Q-switching possono produrre impulsi laser di alta o altissima intensità, utili in numerose applicazioni (industriali e fondamentali)

Tecniche di mode-locking possono produrre impulsi ultra-brevi, utili in molti metodi di analisi (e anche per applicazione, ad esempio TLC)

# **FONTI**

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